

Kick-off workshop of the HIPOTHEC ANR project. 08/03/2024

Simulation of ultrasonic testing in metallic components J. Dalphin





Sommaire

1. Context

2. Workflow

3. Results

WHY KNO

S. S. MAR



Context

It is a collaboration between different entities of EDF R&D:

- **ERMES** (J. Dalphin, *P. Thomas*) and
- **MMC** (P.-E. Lhuillier, A. Schumm, Y. Gelebart, S. Wentzel, and Z. Aghenzour)

for the **APEXIS** project financed by Direction Industrielle (**DI**).



The set of techniques and processes giving informations about the health of a component or a structure, without resulting in any harmful alterations to their uses are gathered under two principal appelations: non-destructive testing (NDT) or non-destructive examinations.

Created in 1967, the **COFREND**, Confédération Française pour les Essais Non Destructifs, is the reference entity in the domain of Certification and Qualification of agents in France for non-destructive testings and evaluations.



The object of NDT is to determine with reliability and at the appropriate scale of observations the presence and the nature of defects in components.

In the specific context of EDF SA: NDT are the main techniques the operator disposes to guarantee the components integrity, in addition to the design and manufacturing ones.

This requirement of detecting defects as soon as they represent a security threat of components integrity of pressurized water nuclear reactor is enforced by law (arrêté du 10/11/1999). It is one of the main purposes of the operator.









In the field of **metallic components** they are three main types of NDT:

➢ Eddy-currents

- > Ultrasounds
- $\succ Radioagraphy (\preceq 2027)$



CODE The methodology of the ultrasonic NDT laboratory



The methodology of the ultrasonic NDT laboratory

Fundamental expertise of the ultrasonic NDT laboratory:

→ link between the metallurgic structure of components and their controlability by ultrasounds.



General method - Experimence

edf



edf



1. The tools for the characterization of materials



General methodology - Simulation

- → Simulation codes are essential tools for engineers to enhance the reliability of diagnostics for NDT inspections and the demonstration of performances. Internal softwares are available for the three types of NDT at EDF R&D
- → In the qualification process of NDT, simulations allow to evaluate the impact of influent parameters, limiting the number of experiments.

Caracterization

Experience



- → Detection of realistic defects by numerical simulations.
- → Propagation of 3D ultrasonic waves in an elastic media.
- → Remplace ATHENA3D by a industrial tools to help engineers to make decision.
- → Be compatible with the already-existing tools of pre- and post-processing treatements.



- Treat arbitrary geometry with potential complex defects.
- Elastodynamics in heterogeneous anisotropic media.
- Performance et reliability greater than ATHENA3D.
- Easy code maintenance and ergonomy of use for engineers.
- Compatibily with MILENA, SALOME and PARAVIS.

Desired specifications with respect to the new solver called A3D-CND.

Cedf











Comparison of performances between a Fortran short code (P. Thomas) et code_aster on a PFC.



First successfull connection between A3D-CND (written in C) and MILENA (C++) on a isotropic screw of the nuclear pressure vessel.



Simulation over granular microstructures highly anisotropic and heterogeneous like a numerical real three-pass weld (NEMESIS).





Workflow

Strong physical and numerical constraints:

- **Simplify** methods as much as one can;
- Gain **time** in software development.



2.0 Typical workflow of an ultrasonic inspection

PHASE 0 (preparation): machining or generation of the component to inspect

PHASE 1 (emission): creation of an ultrasonic signal and propagating it up to the boundary of the object to inspect
PHASE 2 (inspection): propagate the signal inside the material with complex properties and arbitrary geometry
PHASE 3 (reception): recording the part of the signal that will propagate up to the sensors (A-Scan).



2.0 Typical workflow for the simulation of an ultrasonic inspection





edr

2.1 The physical constraint

The **size** of the defect one aims to detect **determine** the minimal **frequency** of the incident wave sent by the emission sensor:

• frequency_minimal = speed_waveP_steel / 2 size_defect.

Example: A defect of 1 mm imposes a central frequency of 6 MHz (with 50% bandwidth) for the emission sensor.





2.2 The spatial numerical discretization constraint

Spatial discretization must correctly approximate the incident waves.

The **frequency** of the incident wave **determine** the **maximal edge length** possible inside the mesh:

• Length_max = speed_wave / 12 frequency_max

Example: 60 micrometers maximum for 6 MHz.





2.3 The time discretization numerical constraint



<u>Condition CFL (Courant-Friedrich-Levy)</u>: roughly speaking, the time necessary for any physical wave to travel over one tetrahedra in the worst case cannot be lower than the numerical time step.

The **minimal edge length** possible inside the mesh **determine** the maximal **time step**:

Time_step_max = 0.5 length_min
 / speed_waveP_steel.
 23

Example: 2 ns for 10 micrometers.



<u>Numerician:</u> yes, but that implies a space discretization step of 50 micrometers, hence a mesh of **24 billions of tetraedra** (and 4 billions of nodes) for 5000 iterations of 8 ns.

About the number of tetraedra:

- Coarse mesh: 400 millions
- Usual mesh: 1 milliard
- Fine mesh: 10 milliards

Software development choice:

- Re-implementation ex-nihilo
- A solution using code_aster

Bet made on the solver A3D-CND:

- P1 finite element for space discretization, explicit Euler scheme for the time discretization
- Parallelization with **OpenMP** of the time loop.

 $U_{m+1} = U_m + \Delta t \, \dot{U}_m$ $\dot{U}_{m+1} = \dot{U}_m + \Delta t \, M^{-1} \left[G_{m+1} + F_{m+1} - K U_{m+1} \right].$



3

Results

Two typical studies are considered for qualitative results:

- Simulate for a potentially little defect (7 MHz) on a complex geometry (crew) with homogeneous **isotropic** material.
- Simulate for potentially **coarser defects** (2 MHz) on granular objects (weld) with simple geometry but highly **heterogeneous** and/or **anisotropic** material.



3.1 Results obtained for a crew in 2021



Mesh of a screw with specifications (23,8mm)x(23,8mm)x(69,55mm):

- Nb nodes (= nb dof) ~ 40 millions
- Nb tetra ~ 225 millions
- Nb coef ≠0 matrix ~ 570 millions

Length of edges in the mesh:

- Minimal = 26 micrometers
- Mean = 84 micrometers
- Maximal = 153 micrometers

Numerical constraints:

- Central frequency < 4,2 MHz
- Time step < 4,4 ns
- Defect size ~ 1 mm







- Central frequency used for the emission: 4 MHz
- Source used: punctual and inclinated
- Sampling frequency: 500 MHz
- RAM used : 60 GB
- Standard node (cn) onthe old cluster with 28 cpus
- Computational time: 2h53 = 27 min (initialization) + 4 000 iter x 2,19 sec



Norm of the velocity inside a plane cut of the screw



5





3.2 Results obtained for a three-pass weld in 2022



Mesh of an anisotropic heterogeneous grid (14mm)x(10mm)x(10mm):

- Nb nodes (=nb dof) ~ 175 millions
- Nb tetra ~ 1 billion
- Nb coef ≠0 matrix ~ 2.5 billions

Length of edges in the mesh:

- Minimal=20 micrometers
- Mean=26 micrometers
- Maximal=35 micrometers

Numerical constraints:

- Source frequency < 4.8 MHz
- Time step < 3,3 ns
- Taille défaut ~ 1 mm





- Different frequencies used for a sensor in immersion
- Time of the simulation:
 6,4 μs
- Sampling frequency: 625 MHz
- RAM used : 340 GB
- Big memory node (bm) on the new cluster with 24 cpus
- Computation time: 5h30 (4 000 iterations)



$\int f_{cen} \left(MHz \right)$	$h_w (mm)$
2	90
5	160
7.5	250

Configuration of the NEMESIS simulation



CDF Norm of the velocity in the visualization plane for different frequencies



Norm of the velocity in the visualization plane for different frequencies at t=1,7 μ s





- -----

-