

Stochastic modeling and hydrostatic balance

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- Strong interest on the use of stochastic filters and ensemble methods for data assimilation and forecasting

⇒ Require stochastic version of the evolution law and/or a modeling of the dynamics errors

Several frameworks proposed in the literature (Berner et al 2017, Franzke et al. 2015)

- additive/multiplicative forcing (Buiza et al 99), backscattering (Leight 71), (Mason and Thomson 92)
- Low/fast modes decomposition (Majda et al. 99, Franzke et al 05), scale separation (Grooms and Majda).
- Approaches based on stochastic transport (Holm 15, Mémin 14)

Location Uncertainty (LU) Principles

- Stochastic flow :

$$d\mathbf{X}_t = \underbrace{\mathbf{u}(\mathbf{X}_t, t)dt}_{\text{large-scale / resolved}} + \underbrace{\boldsymbol{\sigma}(\mathbf{X}_t, t)d\mathbf{B}_t}_{\text{small-scale / unresolved}}$$

- Functional process :

$$\boldsymbol{\sigma}(\mathbf{x}, t)d\mathbf{B}_t = \int_{\Omega} \check{\boldsymbol{\sigma}}(\mathbf{x}, \mathbf{y}, t)d\mathbf{B}_t(\mathbf{y})d\mathbf{y}$$

B_t functional cylindrical Wiener process and $\check{\boldsymbol{\sigma}}$ is a bounded deterministic symmetric kernel $\Rightarrow \boldsymbol{\sigma}$ Hilbert-Schmidt

- Spectral decomposition

$$\boldsymbol{\sigma}(\mathbf{x}, t)d\mathbf{B}_t = \sum_{n \in \mathbb{N}} \boldsymbol{\Phi}_n(\mathbf{x}, t)d\beta_t^n$$

- Covariance operator :

$$\begin{aligned} Q(\mathbf{x}, \mathbf{y}, t, s) &= \mathbb{E} \left[\boldsymbol{\sigma}(\mathbf{x}, t) d\mathbf{B}_t (\boldsymbol{\sigma}(\mathbf{y}, s) d\mathbf{B}_s)^T \right] \\ &= \delta(t - s) dt \int_{\Omega} \check{\boldsymbol{\sigma}}(\mathbf{x}, \mathbf{z}, t) \check{\boldsymbol{\sigma}}^T(\mathbf{y}, \mathbf{z}, s) d\mathbf{z} \end{aligned}$$

- Variance tensor (per unit of time) :

$$\mathbf{a}(\mathbf{x}, t) dt = Q(\mathbf{x}, t)$$

- Turbulent Kinetic Energy (TKE) :

$$\text{TKE} = \frac{1}{2} \frac{\text{tr}(\mathbf{a})}{dt} \quad (m^2 \cdot s^{-2})$$

Stochastic Reynolds Transport Theorem (SRTT)

We assume that $\nabla \cdot \boldsymbol{\sigma} = 0$ in the following.

- Rate of change of a scalar process θ within a volume transported by the stochastic flow :

$$d \int_{\mathcal{V}(t)} \theta(\mathbf{x}, t) d\mathbf{x} = \int_{\mathcal{V}(t)} (D_t \theta + \theta \nabla \cdot \mathbf{u}^*) d\mathbf{x}$$

- Stochastic transport operator :

$$D_t \theta \triangleq d_t \theta + \underbrace{\left(\mathbf{u} - \frac{1}{2} \nabla \cdot \mathbf{a} \right)}_{\mathbf{u}^* = \mathbf{u} - \mathbf{u}_s} \cdot \nabla \theta dt + \underbrace{\boldsymbol{\sigma} dB_t \cdot \nabla \theta}_{\text{multiplicative noise}} - \underbrace{\nabla \cdot \left(\frac{\mathbf{a}}{2} \nabla \theta \right)}_{\text{subgrid diffusion}} dt$$

$\mathbf{u} - \mathbf{u}_s$: corrected drift – effect of statistical inhomogeneity of the small-scale flow component; generalization of the Stokes drift; transitional regime (buffer zone in boundary layer turbulence)

[Bauer, Chandramouli, Chapron, Li & Mémin 2019a] [Pinier, Mémin, Laizet, & Lewandowski 2019]

For incompressible flow (with $\nabla \cdot \mathbf{u}^* = 0$)

- Conservation of passive scalar :

$$D_t \theta = 0$$

- Conservation of tracer energy : [Resseguier, Memin & Chapron, 2017a]

$$d \int_{\Omega} \frac{1}{2} \theta^2 = \int_{\Omega} \theta d_t \theta + \frac{1}{2} d \langle \theta, \theta \rangle_t = 0$$

- Energy decomposition in terms of mean and variance fields :

$$0 = \frac{d}{dt} \int_{\Omega} \frac{1}{2} (\mathbb{E}[\theta])^2 + \frac{d}{dt} \int_{\Omega} \frac{1}{2} \text{Var}[\theta]$$

Stochastic Navier-Stokes Equations (SNS)

- Momentum equation:

$$D_t \mathbf{u} + \mathbf{f} \times (\mathbf{u} dt + \boldsymbol{\sigma} d\mathbf{B}_t) = \mathbf{g} dt - \frac{1}{\rho} \nabla (p dt + dp_t^\sigma) + \nu \nabla^2 (\mathbf{u} dt + \boldsymbol{\sigma} d\mathbf{B}_t)$$

- Continuity equation:

$$\nabla \cdot (\mathbf{u} - \mathbf{u}_s) = 0, \quad \nabla \cdot \boldsymbol{\sigma} = 0$$

- Mass equation:

$$D_t \rho = 0$$

Stochastic Simple Boussinesq Equations (SSBE)

Weak compressibility: $\rho(\mathbf{x}, t) = \rho_0 + \delta\rho(\mathbf{x}, t)$ and $p(\mathbf{x}, t) = p_0(z) + \delta p(\mathbf{x}, t)$

Hydrostatic balance: $\frac{\partial p_0}{\partial z} = -g\rho_0$

- Horizontal momentum equation:

$$D_t \mathbf{u}^h + f \mathbf{k} \times (\mathbf{u}^h dt + \boldsymbol{\sigma} d\mathbf{B}_t^h) = b \mathbf{k} - \nabla_h (\phi dt + d\phi_t^\sigma)$$

- Vertical momentum:

$$D_t w = -\frac{\partial}{\partial z} (\phi dt + d\phi_t^\sigma) + b dt$$

- Continuity equation:

$$\nabla \cdot (\mathbf{u} - \mathbf{u}_s) = 0, \quad \nabla \cdot \boldsymbol{\sigma} = 0$$

- Buoyancy equation:

$$D_t (b + N^2 z) = 0$$

$\phi = \delta p / \rho_0$ and $d\phi_t^\sigma = dp_t^\sigma / \rho_0$: rescaled pressure fluct., $b = -g\delta\rho/\rho_0$: buoyancy

Stochastic Simple Boussinesq Equations (SSBE)

Adimensionnal buoyancy equation:

$$\begin{aligned} (d_t b + (\mathbf{u} - \frac{1}{\Upsilon} \mathbf{u}_s) \cdot \nabla b) dt - \frac{1}{2\Upsilon} \nabla \cdot (\mathbf{a} \nabla b) + \frac{1}{\Upsilon^{1/2}} \boldsymbol{\sigma} d\mathbf{B}_t \cdot \nabla b + \\ \frac{1}{Fr^2} \left((w - \frac{1}{\Upsilon} w_s) dt + \frac{1}{\Upsilon^{1/2}} \boldsymbol{\sigma} d\mathbf{B}_{tz} \right) = 0 \end{aligned}$$

Vertical velocity scales as $w \propto Fr^2 U D$, $D = H/L$, $Fr^2 = U^2/N^2 H^2$, $\Phi = f_0 U L$,

$Ro = U/(f_0 L)$, $1/Bu = Fr^2/Ro^2 = L^2/R_d^2$, $\Upsilon = (T \cdot MKE)/(T^\sigma \cdot TKE)$

Vertical momentum equation:

$$\begin{aligned} \frac{Ro}{Bu} D^2 (d_t w + (\mathbf{u} - \frac{1}{\Upsilon} \mathbf{u}_s) \cdot \nabla w) dt - \frac{1}{2\Upsilon} \nabla \cdot (\mathbf{a} \nabla w) dt + \frac{1}{\Upsilon^{1/2}} \boldsymbol{\sigma} d\mathbf{B}_t \cdot \nabla w = \\ (-\partial_z \Phi + b) dt - \partial_z d\phi_t^\sigma \end{aligned}$$

Hydrostatic balance must be discussed w.r.t $\frac{Ro}{Bu} D^2$ and the noise variance $1/\Upsilon$

Hydrostatic balance - I

Horizontal momentum:

$$Ro(d_t \mathbf{u}^h + (\mathbf{u} - \frac{1}{\Upsilon} \mathbf{u}_s) \cdot \nabla \mathbf{u}^h dt - \frac{1}{2\Upsilon} \nabla \cdot (\mathbf{a} \nabla \mathbf{u}^h) dt + \frac{1}{\Upsilon^{1/2}} \sigma d\mathbf{B}_t \cdot \nabla \mathbf{u}^h) + \frac{1}{\Upsilon^{1/2}} \mathbf{f} \times (\mathbf{u}^h + \sigma d\mathbf{B}_t^h) = -\nabla^h \Phi dt - \nabla^h d\Phi_t^\sigma$$

1 Noise regime $\frac{Ro}{Bu\Upsilon^{1/2}} D^2 \ll 1$ and $Ro/\Upsilon^{1/2} \ll 1$, $\nabla \cdot (\sigma d\mathbf{B}_t)^h = 0$ (QG noise)

- Hydrostatic balance:

$$(-\partial_z \Phi + b) dt - \partial_z d\phi_t^\sigma = 0 \implies \underbrace{(\partial_z \Phi = b)}_{HB} \text{ and } \partial_z d\phi_t^\sigma = 0 \text{ i.e. } d\phi_t^\sigma(x, y)$$

- Martingale pressure term

$$\frac{1}{\Upsilon^{1/2}} \mathbf{f} \times \underbrace{\int_{-h}^0 \sigma d\mathbf{B}_t^h dz}_{\widetilde{\sigma d\mathbf{B}_t}} = -\nabla^h d\Phi_t^\sigma h \implies d\Phi_t^\sigma = -\frac{f}{\Upsilon^{1/2} h} \Delta_h^{-1} (\nabla \times \widetilde{\sigma d\mathbf{B}_t})$$

Hydrostatic balance - II

Horizontal momentum:

$$Ro(d_t \mathbf{u}^h + (\mathbf{u} - \frac{1}{\Upsilon} \mathbf{u}_s) \cdot \nabla \mathbf{u}^h) dt - \frac{1}{2\Upsilon} \nabla \cdot (\mathbf{a} \nabla \mathbf{u}^h) dt + \frac{1}{\Upsilon^{1/2}} \boldsymbol{\sigma} d\mathbf{B}_t \cdot \nabla \mathbf{u}^h + \frac{1}{\Upsilon^{1/2}} \mathbf{f} \times (\mathbf{u}^h + \boldsymbol{\sigma} d\mathbf{B}_t^h) = -\nabla^h \Phi dt - \nabla^h d\Phi_t^\sigma$$

2 Noise regime $\frac{Ro}{Bu\Upsilon^{1/2}} D^2 \ll 1$ and $Ro/\Upsilon^{1/2} \ll 1$, $\nabla \cdot (\boldsymbol{\sigma} d\mathbf{B}_t)^h \neq 0$

- Hydrostatic balance:

$$(-\partial_z \Phi + b) dt - \partial_z d\phi_t^\sigma = 0 \implies \underbrace{(\partial_z \Phi = b)}_{HB} \text{ and } \partial_z d\phi_t^\sigma = 0 \text{ i.e } d\phi_t^\sigma(x, y)$$

- Martingale pressure term

$$\text{Helmholtz decomposition: } \frac{1}{\Upsilon^{1/2}} \int_{-h}^0 \boldsymbol{\sigma} d\mathbf{B}_t^h dz = \frac{1}{\Upsilon_g^{1/2}} \widetilde{\boldsymbol{\sigma} d\mathbf{B}_t^g} + \frac{1}{\Upsilon_{ag}^{1/2}} \widetilde{\boldsymbol{\sigma} d\mathbf{B}_t^{ag}}$$
$$\frac{1}{\Upsilon^{1/2}} \mathbf{f} \times \widetilde{\boldsymbol{\sigma} d\mathbf{B}_t} = -\nabla^h d\Phi_t^\sigma h \implies d\Phi_t^\sigma = -\frac{f}{\Upsilon_g^{1/2} h} \Delta_h^{-1} (\nabla \times \widetilde{\boldsymbol{\sigma} d\mathbf{B}_t^g})$$

Hydrostatic balance - III

Horizontal momentum:

$$Ro(d_t \mathbf{u}^h + (\mathbf{u} - \frac{1}{\Upsilon} \mathbf{u}_s) \cdot \nabla \mathbf{u}^h dt - \frac{1}{2\Upsilon} \nabla \cdot (a \nabla \mathbf{u}^h) dt + \frac{1}{\Upsilon^{1/2}} \sigma d\mathbf{B}_t \cdot \nabla \mathbf{u}^h) + \frac{1}{\Upsilon^{1/2}} \mathbf{f} \times (\mathbf{u}^h + \sigma d\mathbf{B}_t^h) = -\nabla^h \Phi dt - \nabla^h d\Phi_t^\sigma$$

3 Noise regime $\frac{Ro}{Bu\Upsilon^{1/2}} D^2 \ll 1$ and $\frac{Ro}{\Upsilon^{1/2}} \propto \mathcal{O}(1)$

- Hydrostatic balance:

$$(-\partial_z \Phi + b) dt - \partial_z d\phi_t^\sigma = 0 \implies \underbrace{(\partial_z \Phi = b)}_{HB} \text{ and } \partial_z d\phi_t^\sigma = 0 \text{ i.e. } d\phi_t^\sigma(x, y)$$

- Modified martingale geostrophic balance

$$\frac{1}{\Upsilon^{1/2}} \sigma d\mathbf{B}_t \cdot \nabla \mathbf{u}^h + \frac{1}{\Upsilon^{1/2}} \mathbf{f} \times \sigma d\mathbf{B}_t^h = -\nabla^h d\Phi_t^\sigma$$

- Martingale pressure term

$$d\Phi_t^\sigma = -\frac{1}{h\Upsilon^{1/2}} \Delta^{-1} \nabla \cdot \int_{-h}^0 (\sigma d\mathbf{B}_t \cdot \nabla \mathbf{u}^h + \mathbf{f} \times \sigma d\mathbf{B}_t^h) dz$$

Hydrostatic balance - IV

Horizontal momentum:

$$Ro(d_t \mathbf{u}^h + (\mathbf{u} - \frac{1}{\Upsilon} \mathbf{u}_s) \cdot \nabla \mathbf{u}^h dt - \frac{1}{2\Upsilon} \nabla \cdot (\mathbf{a} \nabla \mathbf{u}^h) dt + \frac{1}{\Upsilon^{1/2}} \sigma d\mathbf{B}_t \cdot \nabla \mathbf{u}^h) + \frac{1}{\Upsilon^{1/2}} \mathbf{f} \times (\mathbf{u}^h + \sigma d\mathbf{B}_t^h) = -\nabla^h \Phi dt - \nabla^h d\Phi_t^\sigma$$

4 Noise regime $\frac{Ro}{Bu\Upsilon^{1/2}} D^2 \propto \mathcal{O}(1)$

- Hydrostatic balance:

$$-\frac{1}{\Upsilon} \mathbf{u}_s \cdot \nabla w dt - \frac{1}{2\Upsilon} \nabla \cdot (\mathbf{a} \nabla w) dt + \frac{1}{\Upsilon^{1/2}} \sigma d\mathbf{B}_t \cdot \nabla w = (-\partial_z \Phi + b) dt - \partial_z d\phi_t^\sigma \implies$$

- Pressure terms

$$\Phi(z) = \int_{-z}^0 (b + \frac{1}{2\Upsilon} \mathbf{u}_s \cdot \nabla w + \frac{1}{2\Upsilon} \nabla \cdot (\mathbf{a} \nabla w)) dz'$$

$$d\Phi_t^\sigma(z) = \frac{1}{\Upsilon^{1/2}} \int_{-z}^0 \sigma d\mathbf{B}_t \cdot \nabla w dz'$$

$$w(z) = - \int_{-z}^0 (\nabla \cdot \mathbf{u}^h - \frac{1}{\Upsilon} \nabla \cdot \mathbf{u}_s) dz'$$

- Stochastic modelling introduces a relaxation of the classical Hydrostatic assumption
- Schemes for the turbulent pressure computation depends on the noise regime
- High noise regime or high Rossby/Burger flow modifies the hydrostatic balance; it now depends on the Ito-Stokes drift and on the noise diffusion